



# Forecast of the atmospheric parameters at the LBT site in the context of the ALTA project

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# OUTLINE

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Goals of the ALTA projects

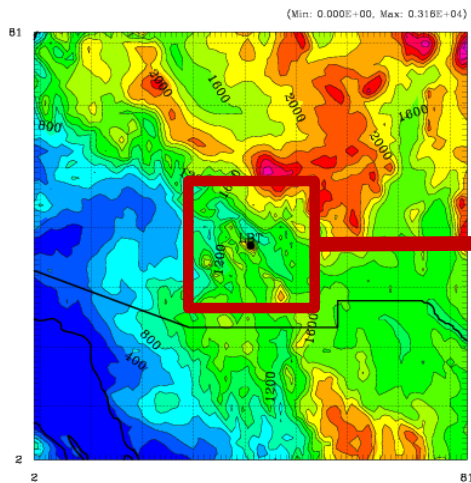
Model configurations in operational setup

Most relevant results of ongoing model validation

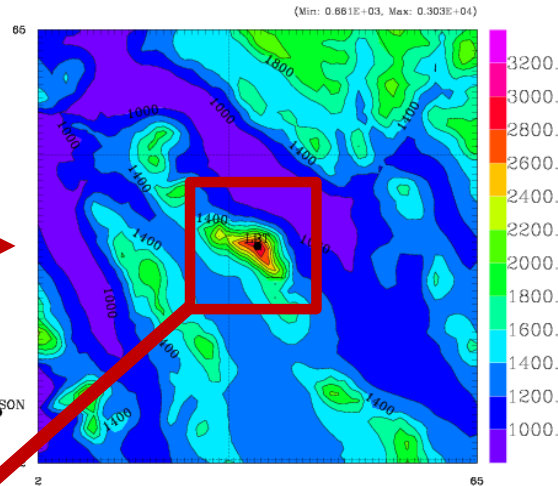
Conclusions

# Model Configuration

800x800km  
 $\Delta X=10\text{km}$

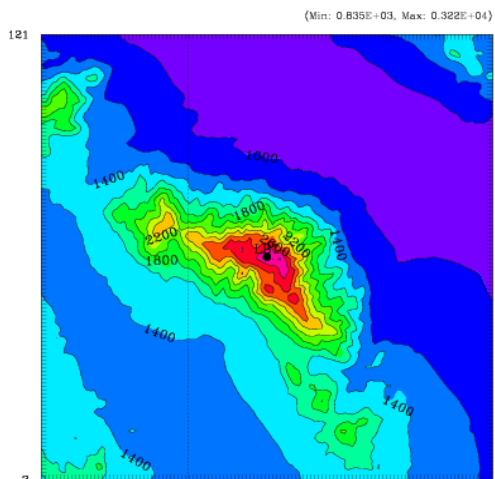


160x160km  
 $\Delta X=2.5\text{km}$



**Astro-MESO-NH**  
mesoscale model

Masciadri et al., A&ASS 1999



60x60km  
 $\Delta X=500\text{m}$

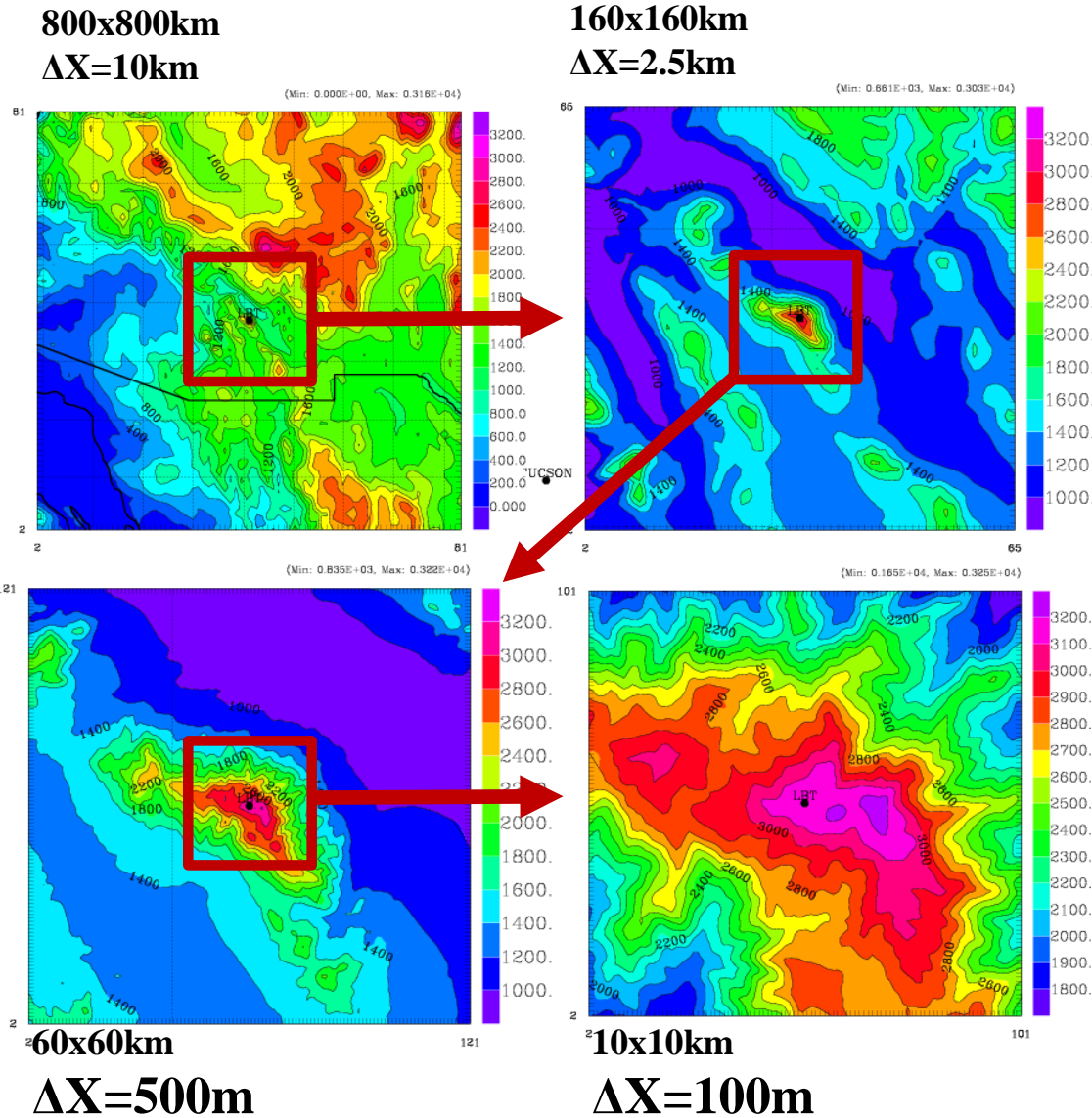


# Model Configuration

## Astro-MESO-NH

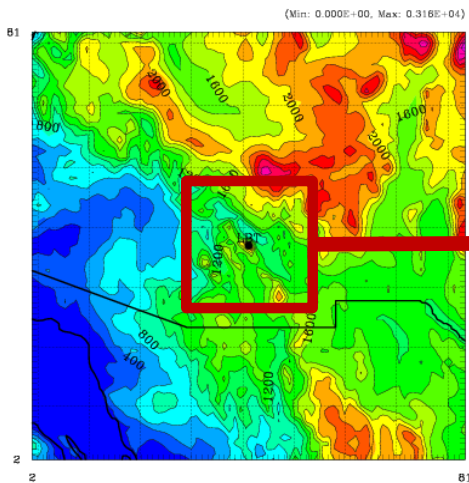
mesoscale model

Masciadri et al., A&ASS 1999

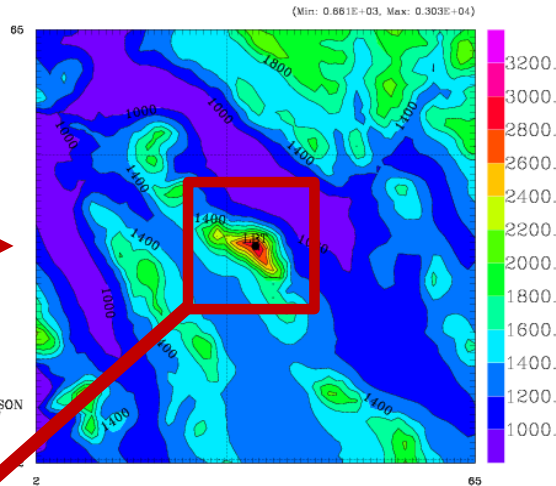


# Model Configuration

800x800km  
 $\Delta X=10\text{km}$



160x160km  
 $\Delta X=2.5\text{km}$

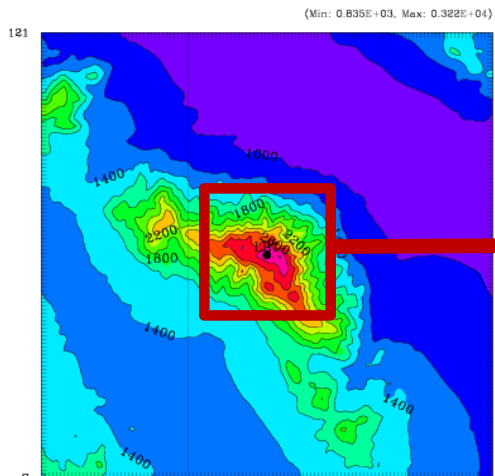


**Astro-MESO-NH**

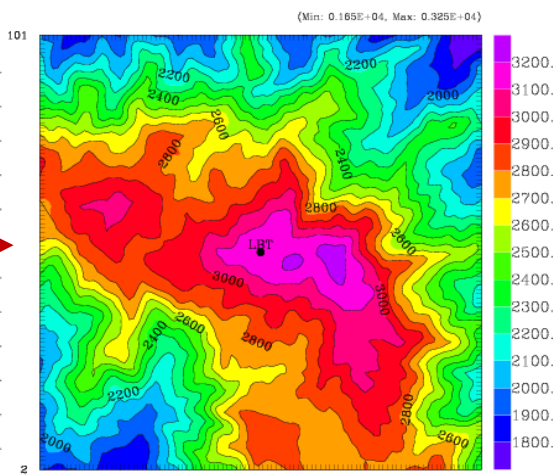
mesoscale model

Masciadri et al., A&ASS 1999

- 54 vertical levels
- $\Delta h_0=20\text{ m}$  (because of trees on orography)
- logarithmic stretching up to 3500m a.g.l.
- for  $h > 3500\text{m}$ ,  $\Delta h \cong 600\text{m}$



60x60km  
 $\Delta X=500\text{m}$



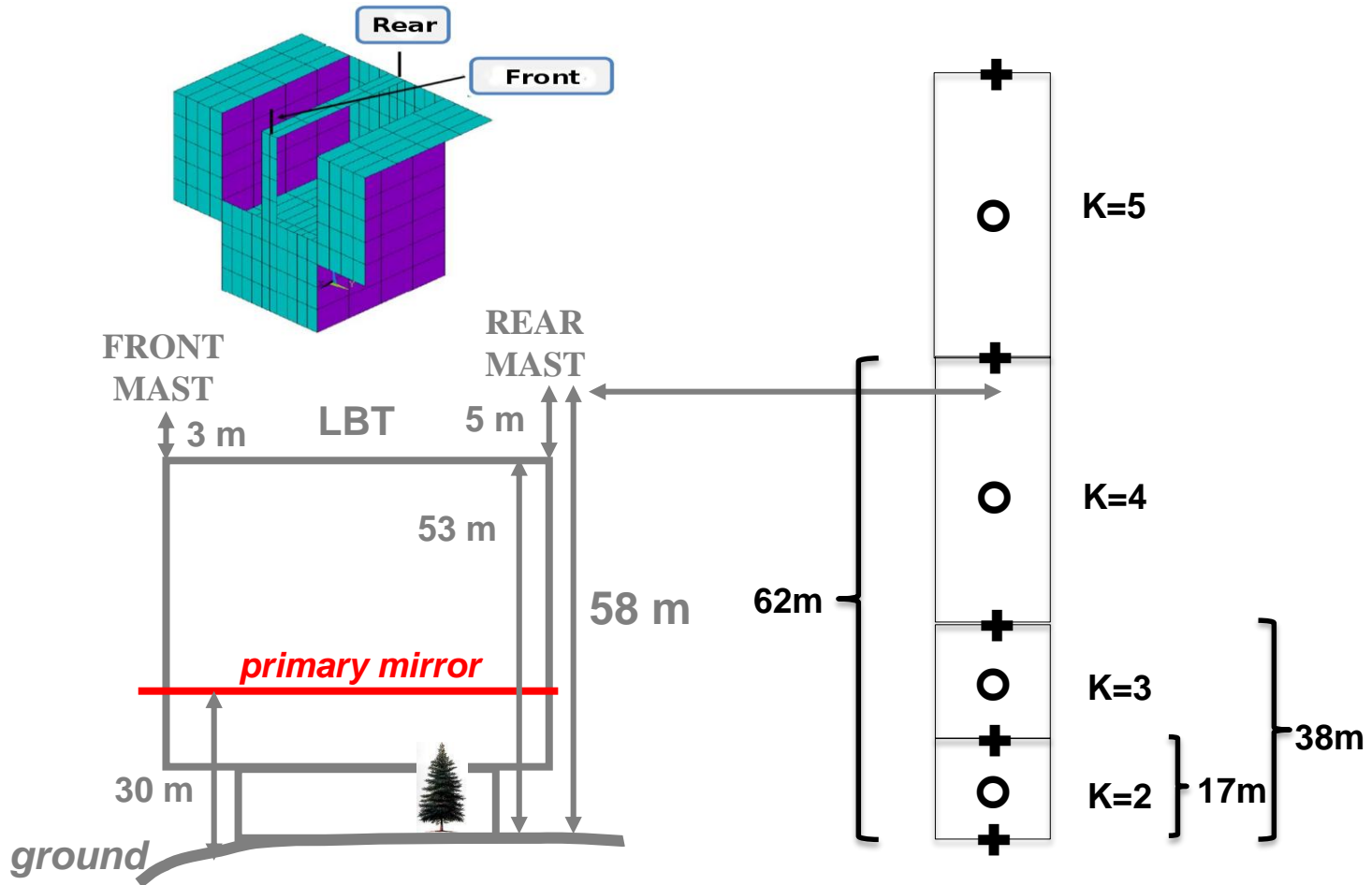
10x10km  
 $\Delta X=100\text{m}$

Temporal sampling:

- Vertical profiles 120s
- Ground values ~1s



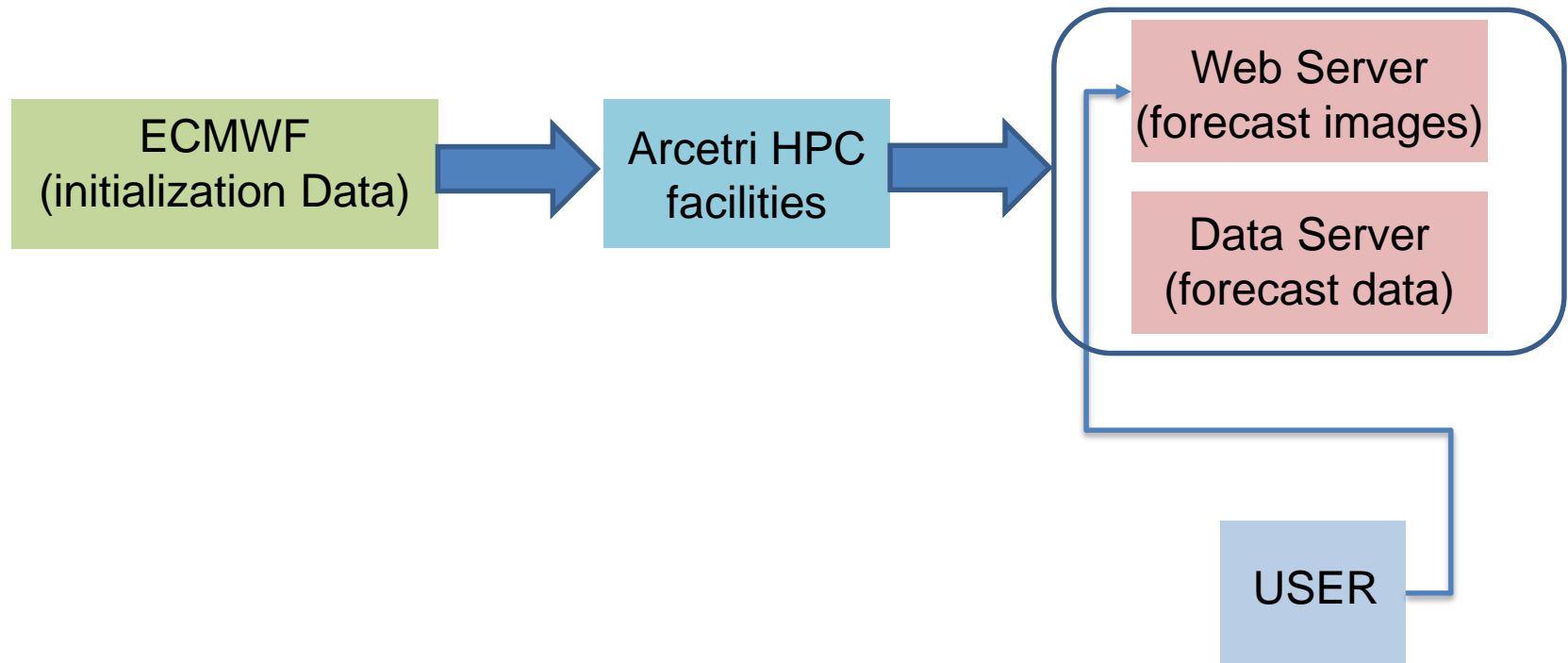
# Model Configuration



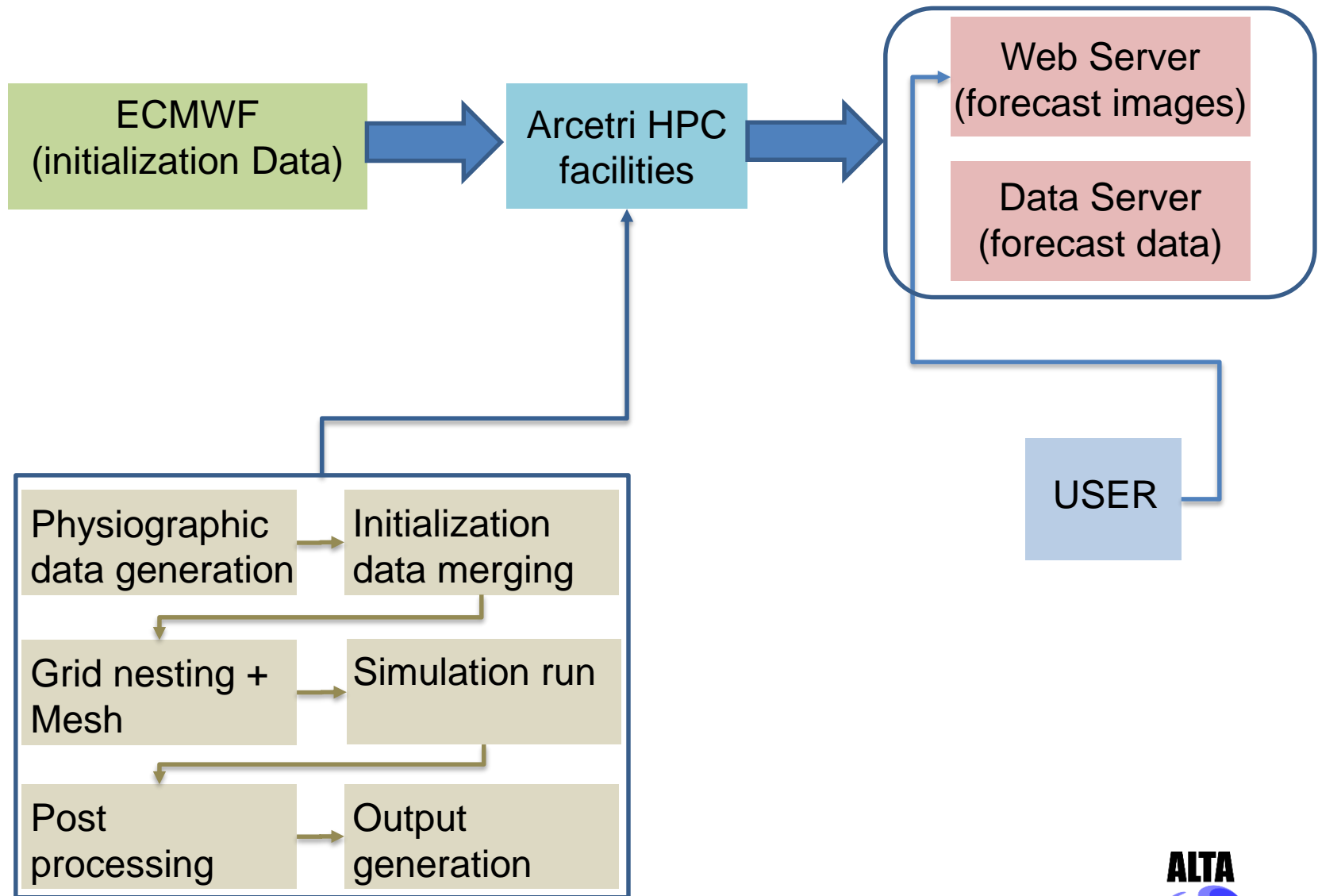
**The model level corresponding to the weather masts is K=4 (38-62m)**

# Operational forecast system overview

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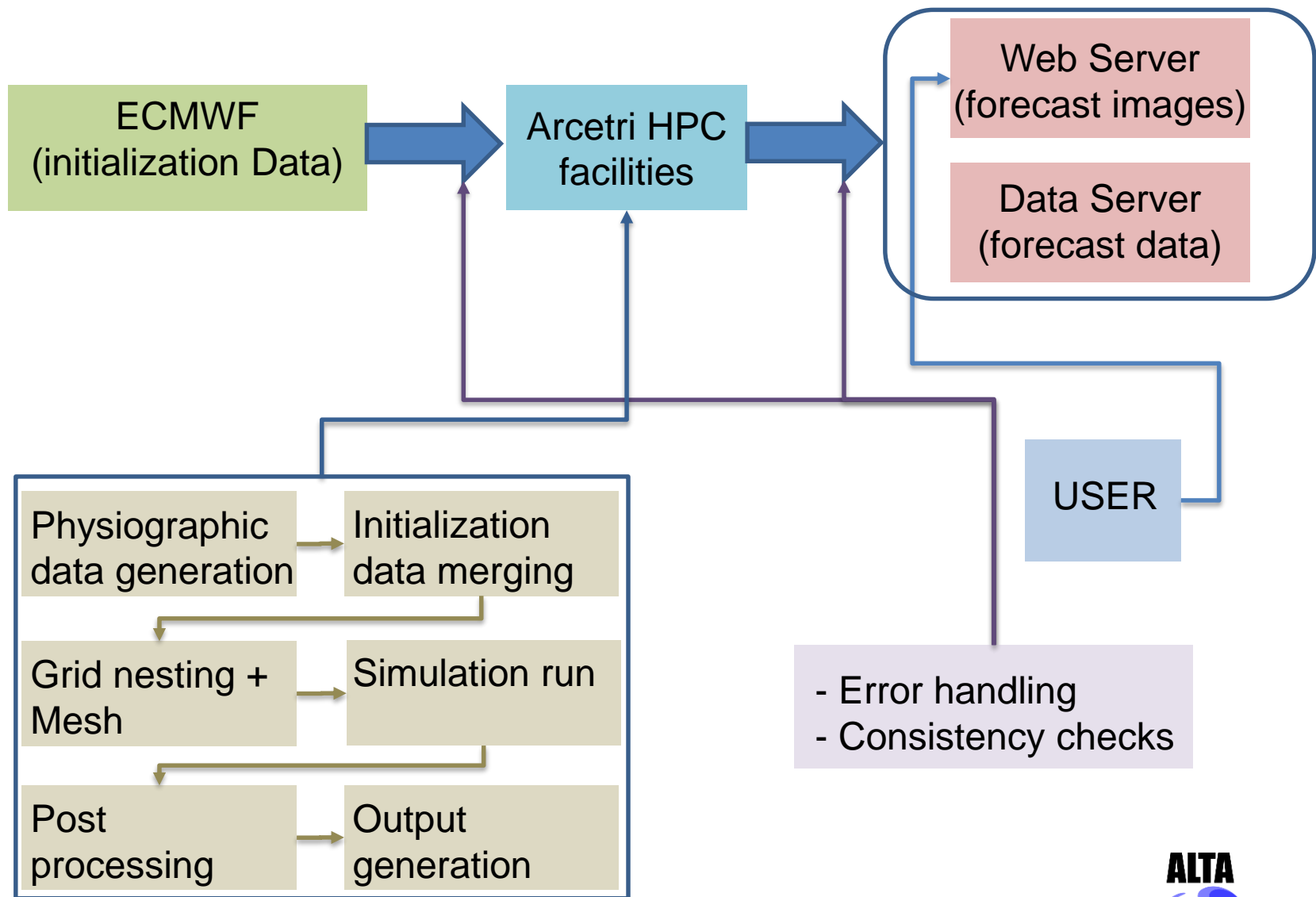


# Operational forecast system overview





# Operational forecast system overview



# Temperature – 3DOM

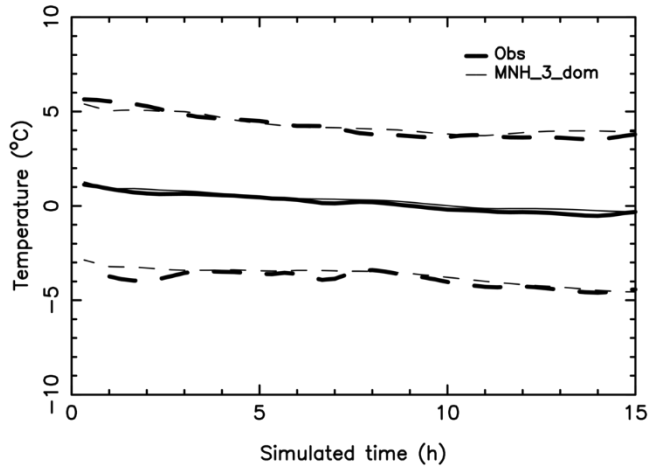
# K=4 Average on 20 nights

## Astro-MESO-NH forecasts (MNH) vs observations (OBS)

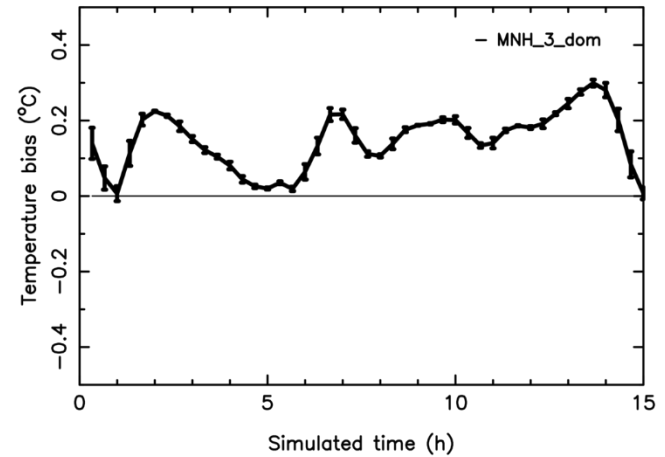
**REAR MAST**

**Sensor height = 55.5m a.g.l.**

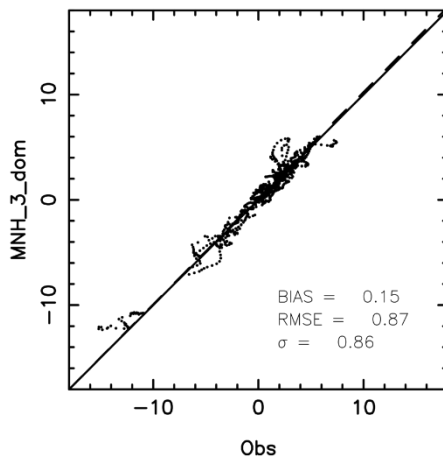
Average Mnh / Obs



Obs

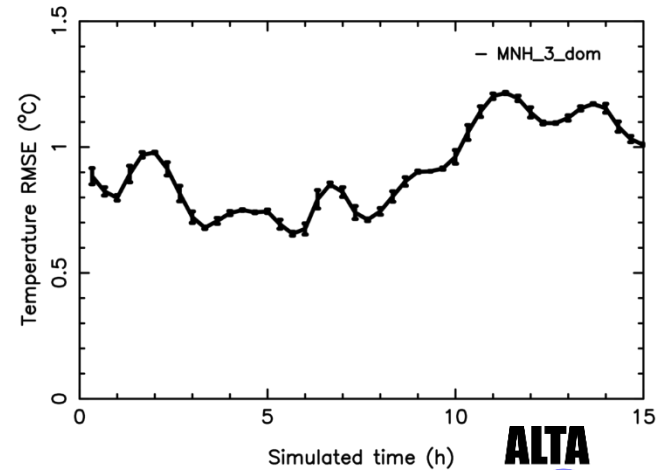


Night Temperature (°C)



**BIAS = 0.15 C°**  
**RMSE = 0.87 C°**  
 **$\sigma = 0.86 C°$**

Obs



# Relative Humidity – 3DOM

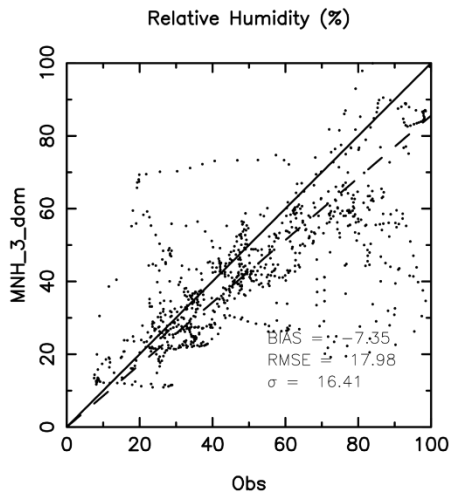
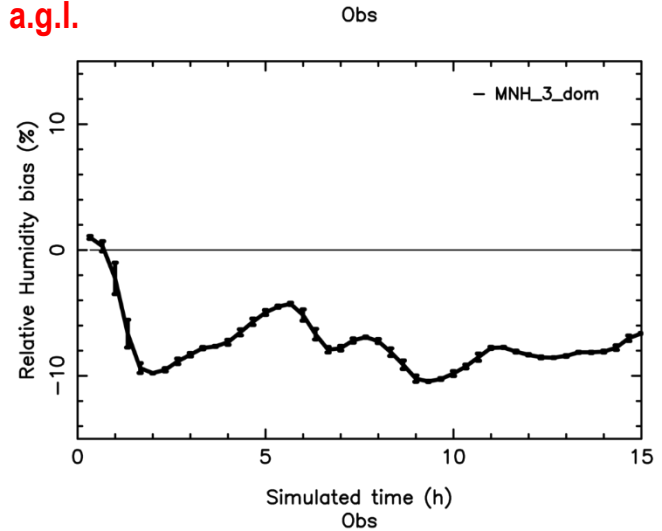
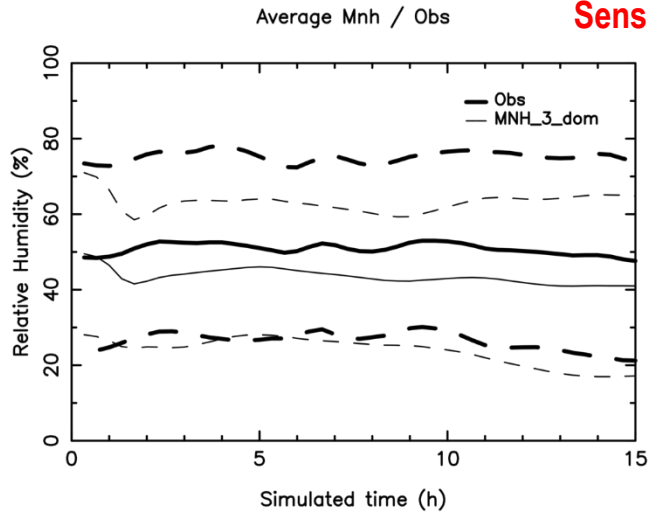
K=4

Average on 20 nights

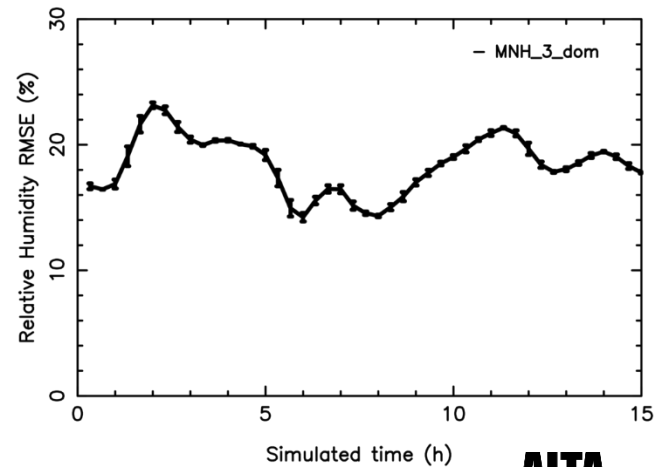
Astro-MESO-NH forecasts (MNH) vs observations (OBS)

REAR MAST

Sensor height =55.5m a.g.l.



BIAS = -7.3%  
RMSE = 18.0%  
 $\sigma$  = 16.4%



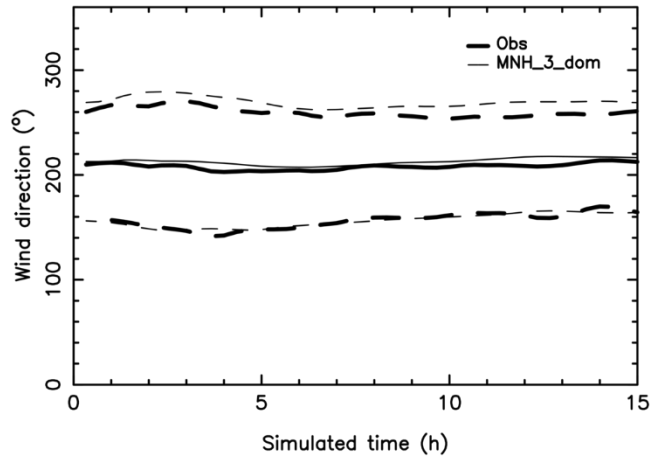
# Wind Direction – 3DOM

**K=4 Average on 20 nights**

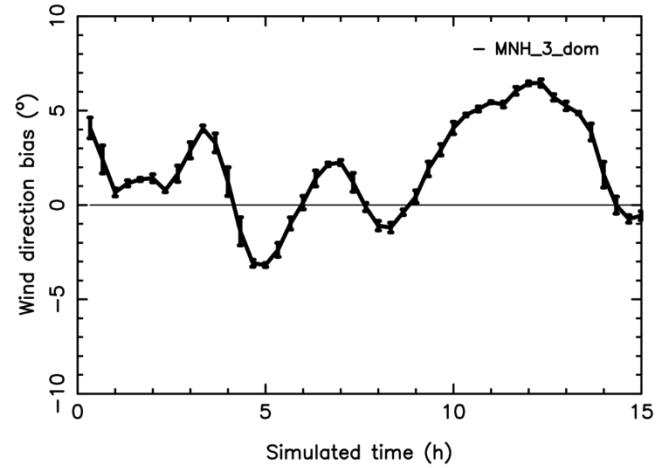
Astro-MESO-NH forecasts (MNH) vs observations (OBS)

**REAR MAST**  
**Sensor height =58m a.g.l.**

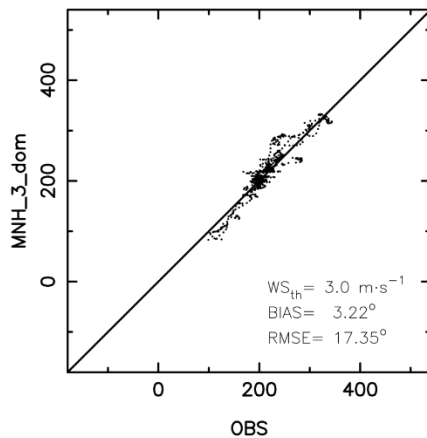
Average Mnh / Obs



Obs



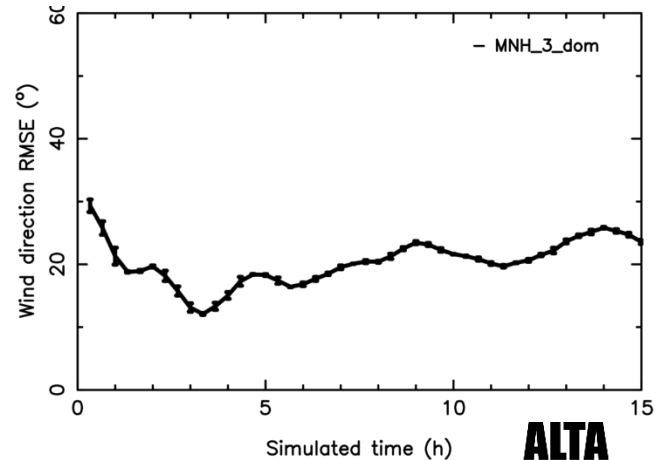
Night wind direction (°)



$$RMSE_{rel} = \frac{RMSE}{180} \times 100 \text{ per cent.}$$

**BIAS = 3.2°**  
**RMSE = 17.3°**  
**RMSE(rel) = 9.6%**

Obs

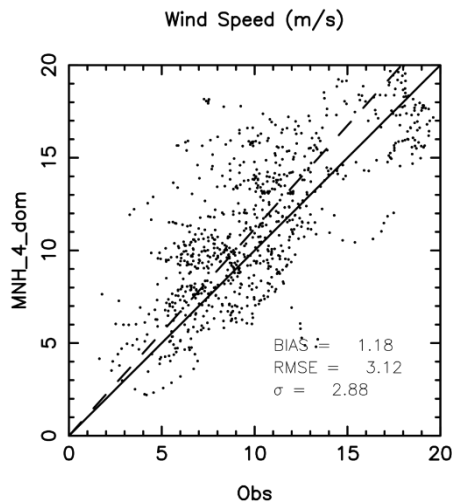
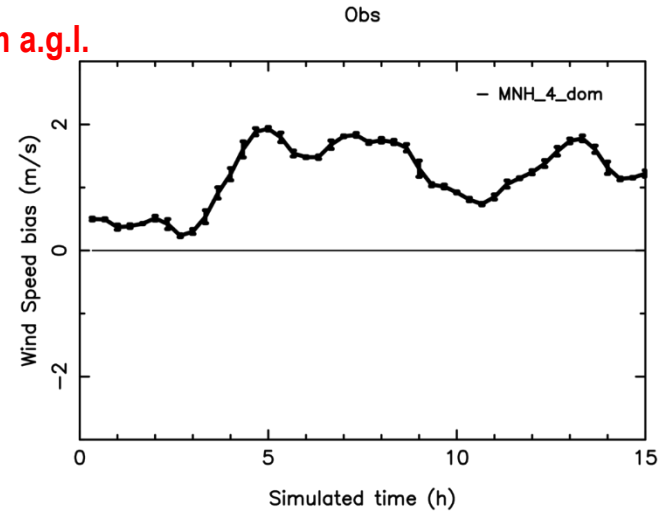
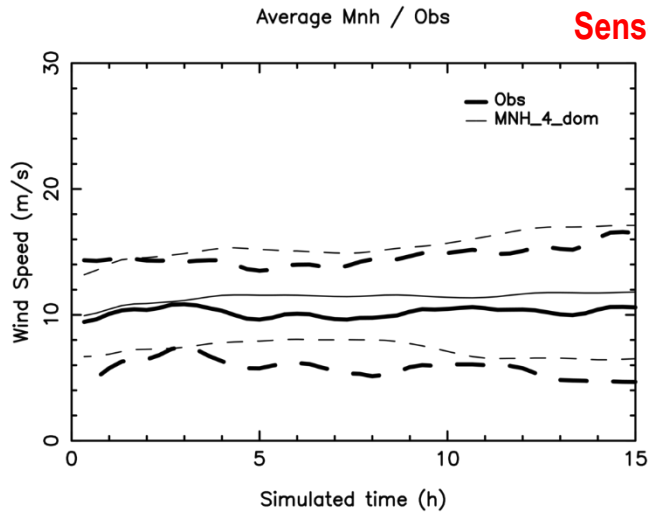


# Wind Speed – 4DOM

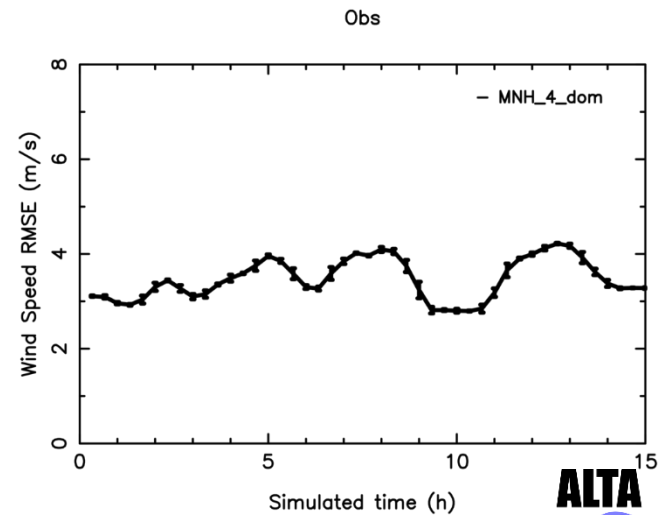
# K=4 Average on 20 nights

Astro-MESO-NH forecasts (MNH) vs observations (OBS)

**REAR MAST**  
**Sensor height =58m a.g.l.**



**BIAS = 1.2 m/s**  
**RMSE = 3.1 m/s**  
 **$\sigma$  = 2.9 m/s**

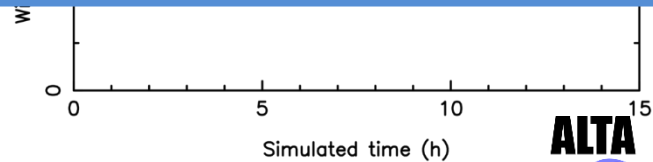
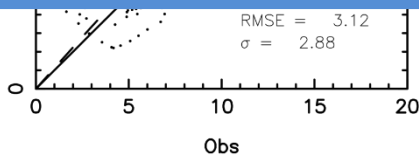
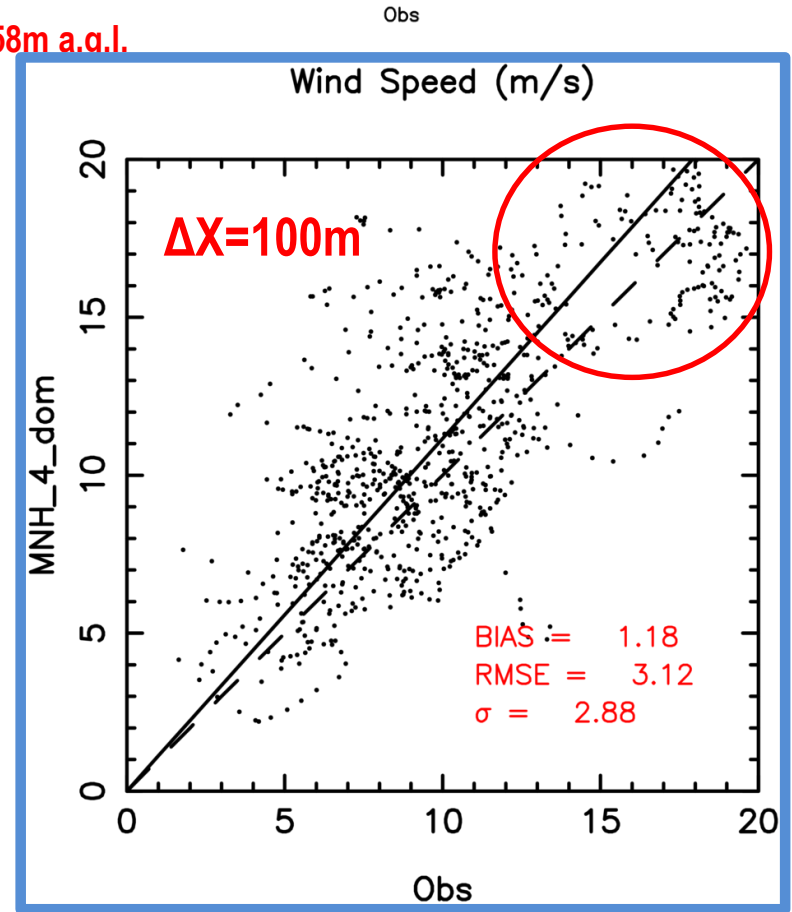
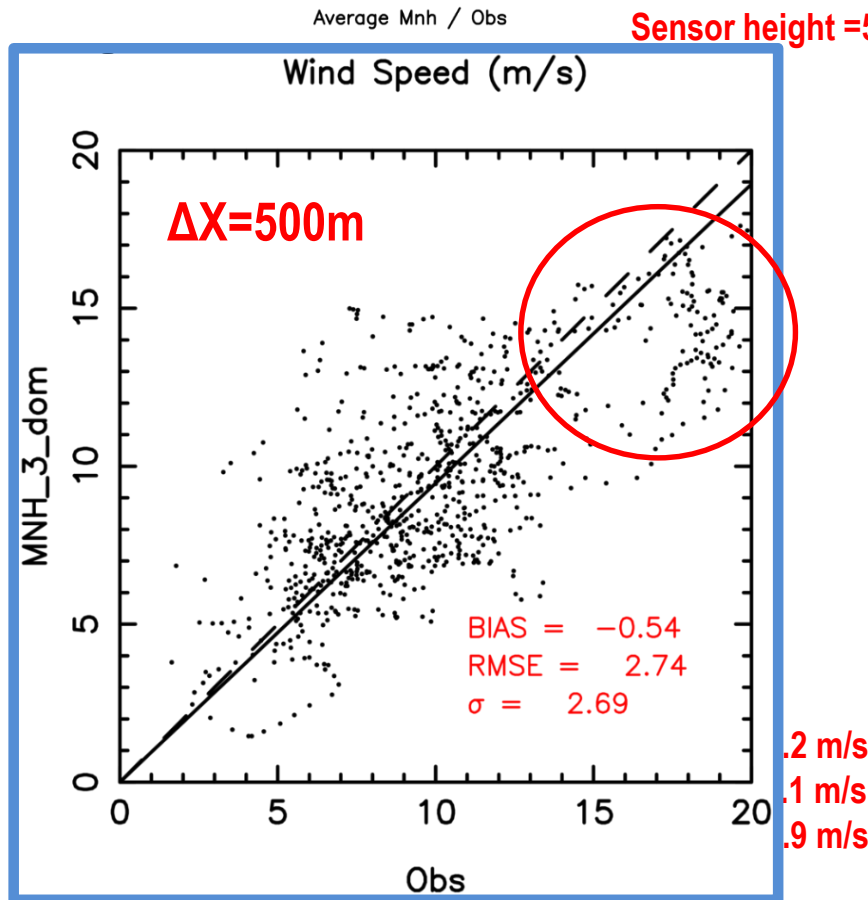


# Wind Speed – 4DOM

# K=4 Average on 20 nights

Astro-MESO-NH forecasts (MNH) vs observations (OBS)

REAR MAST  
Sensor height = 58m a.g.l.



# How to read a contingency table

A contingency table allows for the analysis of the relationship between two or more categorical variables.

Values are divided into categories (e.g. wind <5m/s, 5m/s<wind<10m/s, ....) and a probability to detect each category is computed.

**RANDOM CASE:**  
 PC ~33%  
 POD ~33%  
 EBD ~22%

1.  $PC = (a+e+i)/N * 100$

2.  $POD(1) = a/(a+d+g) * 100$

$POD(2) = b/(b+e+h) * 100$

$POD(3) = c/(c+f+i) * 100$

3.  $EBD = (c+g)/N * 100$

Generic 3 × 3 contingency table.

See Lascaux et. al., MNRAS, 2015

Intervals	Observations			Total
	1	2	3	
<b>Model</b>				
1	<i>a</i> (hit 1)	<i>b</i>	<i>c</i>	<i>a + b + c</i> 1 (Model)
2	<i>d</i>	<i>e</i> (hit 2)	<i>f</i>	<i>d + e + f</i> 2 (Model)
3	<i>g</i>	<i>h</i>	<i>i</i> (hit 3)	<i>g + h + i</i> 3 (Model)
Total	<i>a + d + g</i> 1 (OBS)	<i>b + e + h</i> 2 (OBS)	<i>c + f + i</i> 3 (OBS)	$N = a + b + c + d + e + f + g + h + i$ Total of events



# Temperature and Relative humidity

$\Delta X=500m$

## TEMPERATURE contingency table:

Division by tertiles (climatology) MtG - 55,5m		OBSERVATIONS		
		$T < -1.2^{\circ}C$	$-1.2^{\circ}C < T < 2.5^{\circ}C$	$T > 2.5^{\circ}C$
MODEL	$T < -1.2^{\circ}C$	232	9	0
	$-1.2^{\circ}C < T < 2.5^{\circ}C$	14	342	24
	$T > 2.5^{\circ}C$	7	69	214

**PC = 86.5%**  
**EBD = 0.8%**  
**POD(1) = 91.7%**  
**POD(2) = 81.4%**  
**POD(3) = 90.0%**

Total points = 911;  $PC=86.5\%$ ;  $EBD=0.8\%$   
 $POD_1=91.7\%$ ;  $POD_2=81.4\%$ ;  $POD_3=90.0\%$

## RELATIVE HUMIDITY contingency table:

**PC = 68.4%**

**EBD = 4.4%**

**POD(1) = 81.6%**

**POD(2) = 71.1%**

**POD(3) = 52.5%**

Division by tertiles (climatology) MtG - 55,5m		OBSERVATIONS		
		$RH < 33.9\%$	$33.9\% < RH < 57.7\%$	$RH > 57.7\%$
MODEL	$RH < 33.9\%$	248	80	27
	$33.91\% < RH < 57.7\%$	43	216	117
	$RH > 57.7\%$	13	8	159

Total points = 911;  $PC=68.4\%$ ;  $EBD=4.4\%$   
 $POD_1=81.6\%$ ;  $POD_2=71.1\%$ ;  $POD_3=52.5\%$

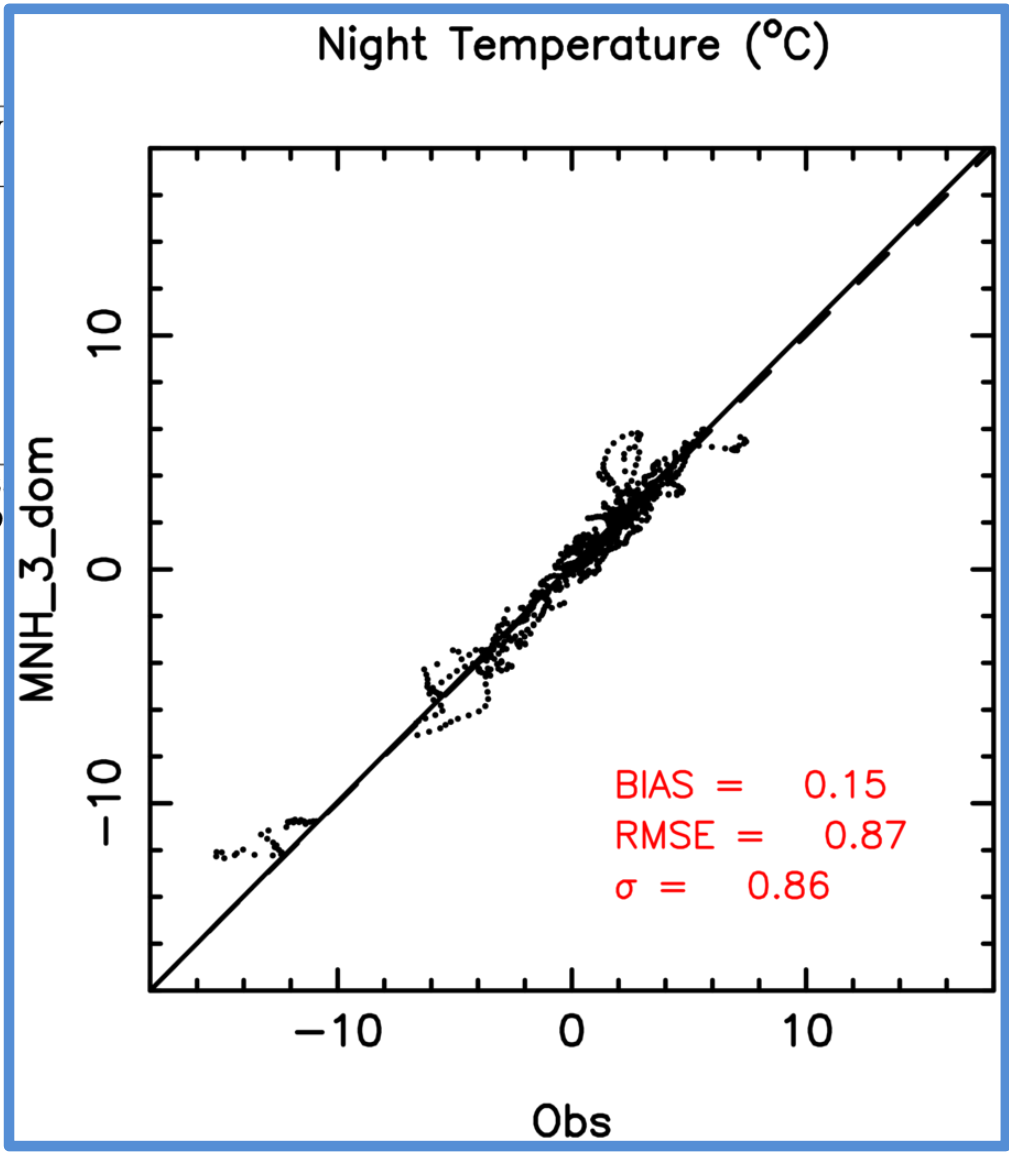




# Temperature and Relative humidity

$\Delta X=500m$

Night Temperature ( $^{\circ}C$ )



**PC = 86.5%**  
**EBD = 0.8%**  
**POD(1) = 91.7%**  
**POD(2) = 81.4%**  
**POD(3) = 90.0%**

TY contingency table:

	OBSERVATIONS		
	<i>RH</i> < 33.9%	33.9% < <i>RH</i> < 57.7%	<i>RH</i> > 57.7%
248	80	27	
43	216	117	
13	8	159	

*BD*=4.4%  
*D*<sub>3</sub>=52.5%



# Temperature and Relative humidity

$\Delta X=500m$

## TEMPERATURE contingency table:

Division by tertiles (climatology) MtG - 55,5m		OBSERVATIONS		
		$T < -1.2^{\circ}C$	$-1.2^{\circ}C < T < 2.5^{\circ}C$	$T > 2.5^{\circ}C$
MODEL	$T < -1.2^{\circ}C$	232	9	0
	$-1.2^{\circ}C < T < 2.5^{\circ}C$	14	342	24
	$T > 2.5^{\circ}C$	7	69	214

**PC = 86.5%**  
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 $POD_1=91.7\%$ ;  $POD_2=81.4\%$ ;  $POD_3=90.0\%$

## RELATIVE HUMIDITY contingency table:

**PC = 68.4%**

**EBD = 4.4%**

**POD(1) = 81.6%**

**POD(2) = 71.1%**

**POD(3) = 52.5%**

Division by tertiles (climatology) MtG - 55,5m		OBSERVATIONS		
		$RH < 33.9\%$	$33.9\% < RH < 57.7\%$	$RH > 57.7\%$
MODEL	$RH < 33.9\%$	248	80	27
	$33.91\% < RH < 57.7\%$	43	216	117
	$RH > 57.7\%$	13	8	159

Total points = 911;  $PC=68.4\%$ ;  $EBD=4.4\%$   
 $POD_1=81.6\%$ ;  $POD_2=71.1\%$ ;  $POD_3=52.5\%$



# Temperature and Relative humidity

$\Delta X=500m$

## TEMPERATURE contingency table

Division by tertiles (climatology)	
MtG - 55,5m	$T < -1.2^{\circ}C$
MODEL	$T < -1.2^{\circ}C$ 232
	$-1.2^{\circ}C < T < 2.5^{\circ}C$ 14
	$T > 2.5^{\circ}C$ 7

Total points = 911;  $PC=86.5\%$ ;  $EBD=0.8\%$   
 $POD_1=91.7\%$ ;  $POD_2=81.4\%$ ;  $POD_3=90.0\%$

**PC = 68.4%**

**EBD = 4.4%**

**POD(1) = 81.6%**

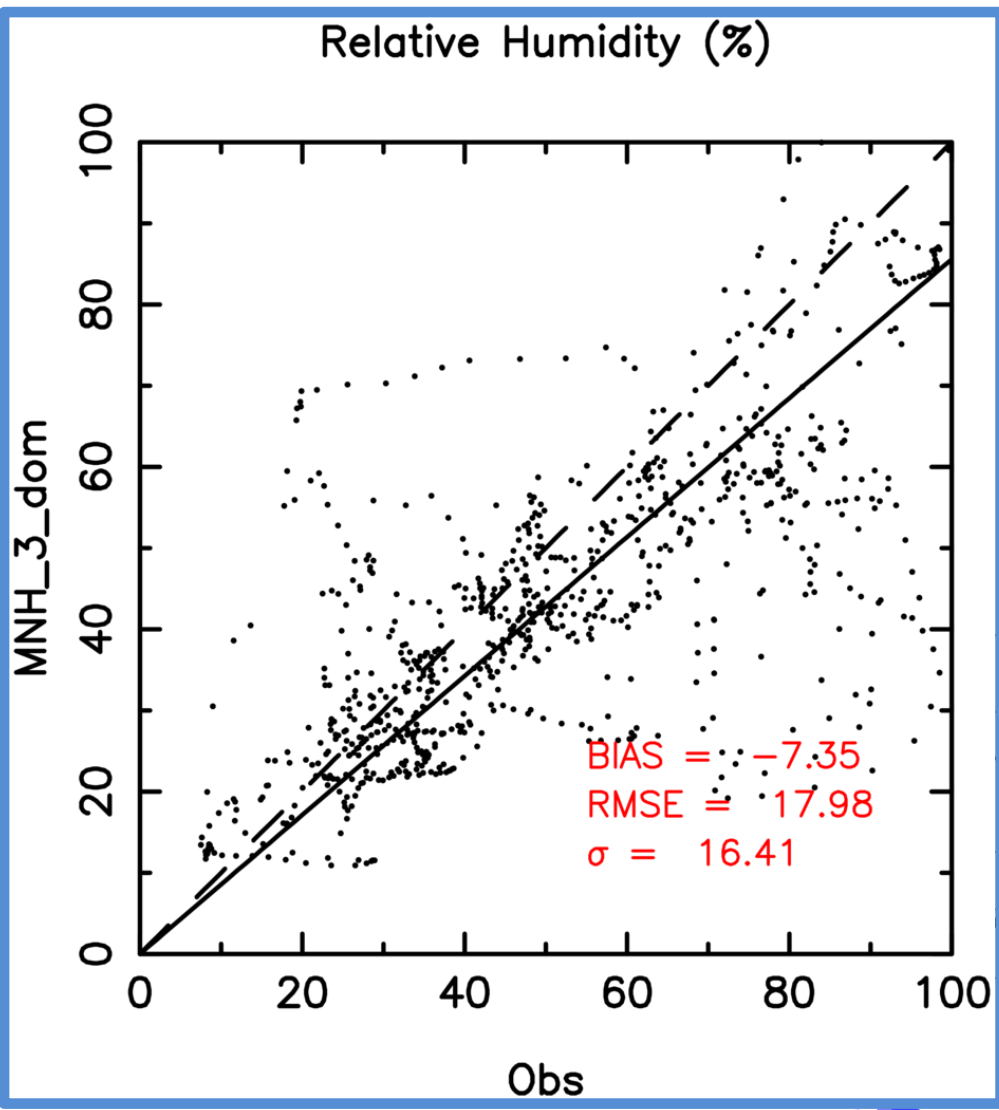
**POD(2) = 71.1%**

**POD(3) = 52.5%**

Division

MODEL

Total p  
 $POD_1=$



57.7%

7

9



# Wind speed, comparison 500m vs 100m resolution

## WIND SPEED contingency table, $\Delta X=500m$

Division by tertiles (climatology) MtG - 58m		OBSERVATIONS		
		$WS < 5.9m/s$	$5.9m/s < WS < 9.7m/s$	$WS > 9.7m/s$
MODEL	$WS < 5.9m/s$	51	32	4
	$5.9m/s < WS < 9.7m/s$	36	242	126
	$WS > 9.7m/s$	14	85	321

**PC = 67.4%**  
**EBD = 2.0%**

**POD(1) = 50.5%**

**POD(2) = 67.4%**

**POD(3) = 71.2%**

Total points = 911;  $PC=67.4\%$ ;  $EBD=2.0\%$   
 $POD_1=50.5\%$ ;  $POD_2=67.4\%$ ;  $POD_3=71.2\%$

## WIND SPEED contingency table, $\Delta X=100m$

**PC = 68.9%**

**EBD = 2.3%**

**POD(1) = 41.6%**

**POD(2) = 60.2%**

**POD(3) = 82.0%**

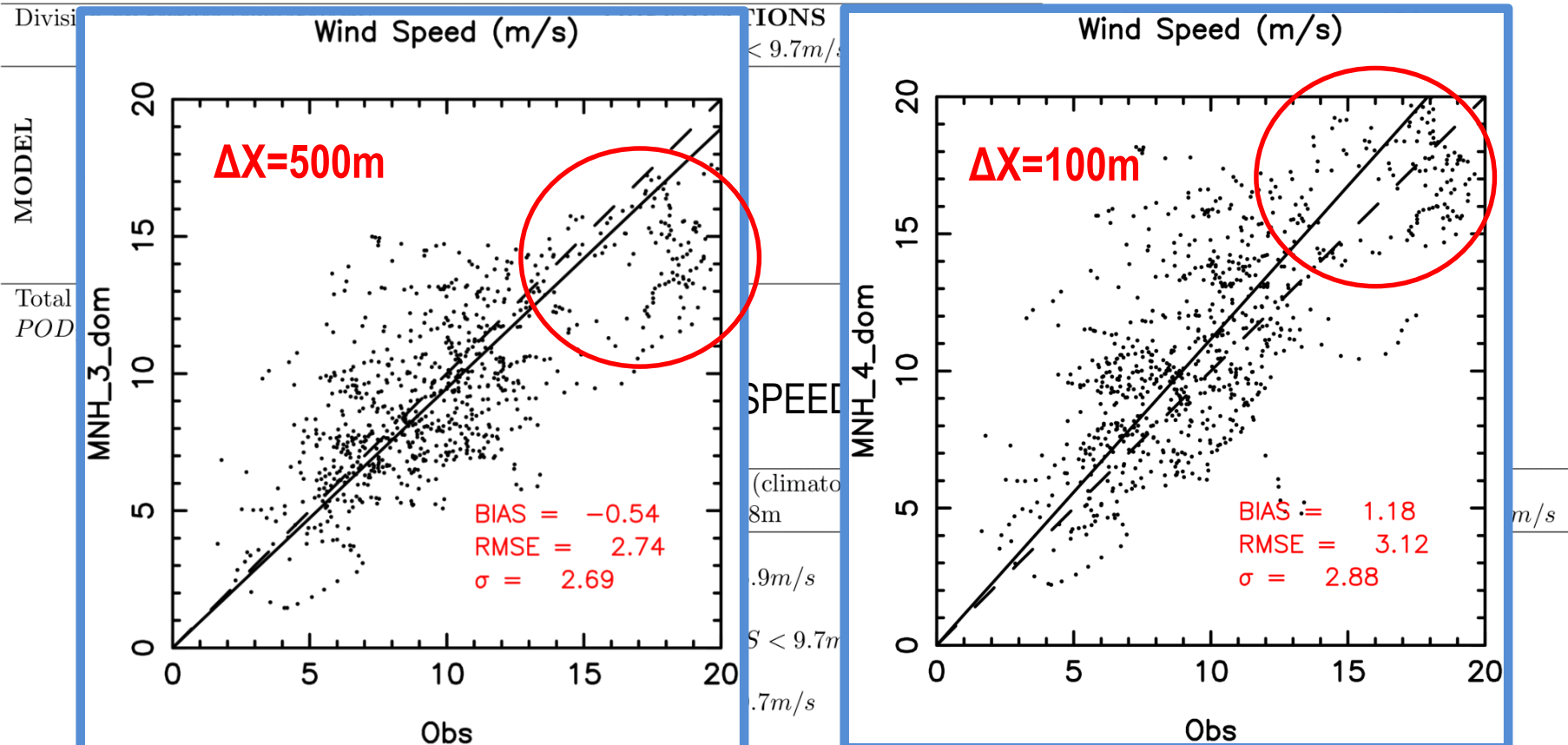
Division by tertiles (climatology) MtG - 58m		OBSERVATIONS		
		$WS < 5.9m/s$	$5.9m/s < WS < 9.7m/s$	$WS > 9.7m/s$
MODEL	$WS < 5.9m/s$	42	25	6
	$5.9m/s < WS < 9.7m/s$	44	216	75
	$WS > 9.7m/s$	15	118	370

Total points = 911;  $PC=68.9\%$ ;  $EBD=2.3\%$   
 $POD_1=41.6\%$ ;  $POD_2=60.2\%$ ;  $POD_3=82.0\%$



# Wind speed, comparison 500m vs 100m resolution

WIND SPEED contingency table,  $\Delta X=500m$



**POD(3) = 82.0%**

Total points = 911; PC=68.9%; EBD=2.3%  
 POD<sub>1</sub>=41.6%; POD<sub>2</sub>=60.2%; POD<sub>3</sub>=82.0%



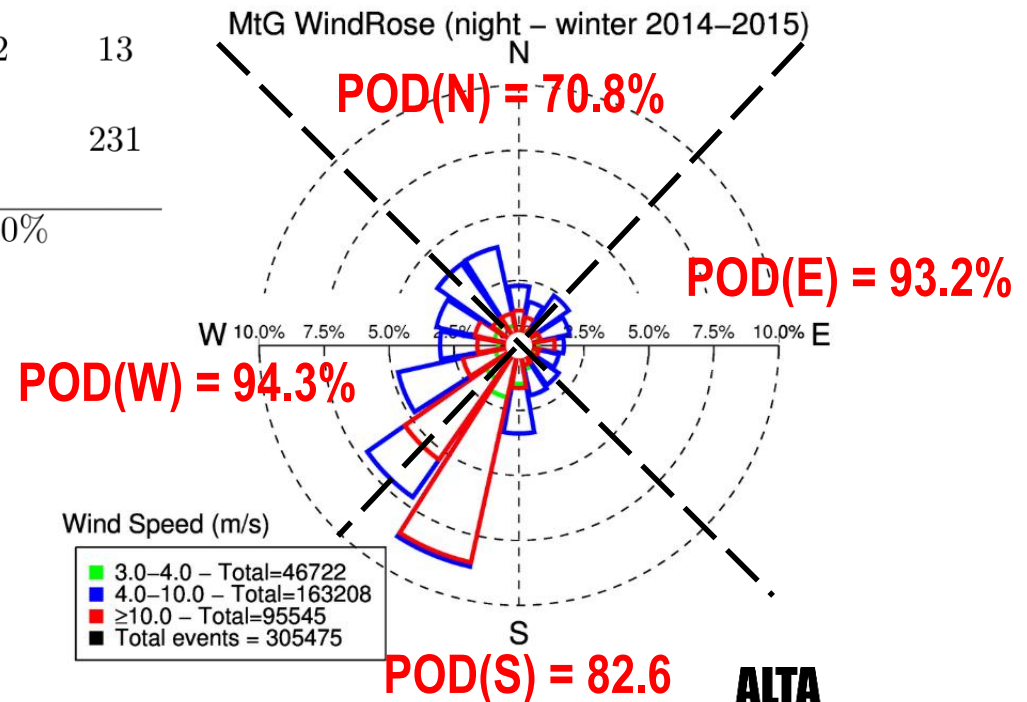
# Wind direction $\Delta X=100\text{m}$

WIND DIRECTION contingency table,  $\Delta X=100\text{m}$

		OBSERVATIONS			
MtG - 58m		N	E	S	W
MODEL	N	34	4	0	1
	E	0	55	12	0
	S	0	0	462	13
	W	14	0	85	231

Total points = 911;  $PC=85.8\%$ ;  $EBD=0\%$   
 $POD(N)=70.8\%$ ;  $POD(E)=93.2\%$   
 $POD(S)=82.6\%$ ;  $POD(W)=94.3\%$

**PC = 85.8%**  
**EBD = 0%**

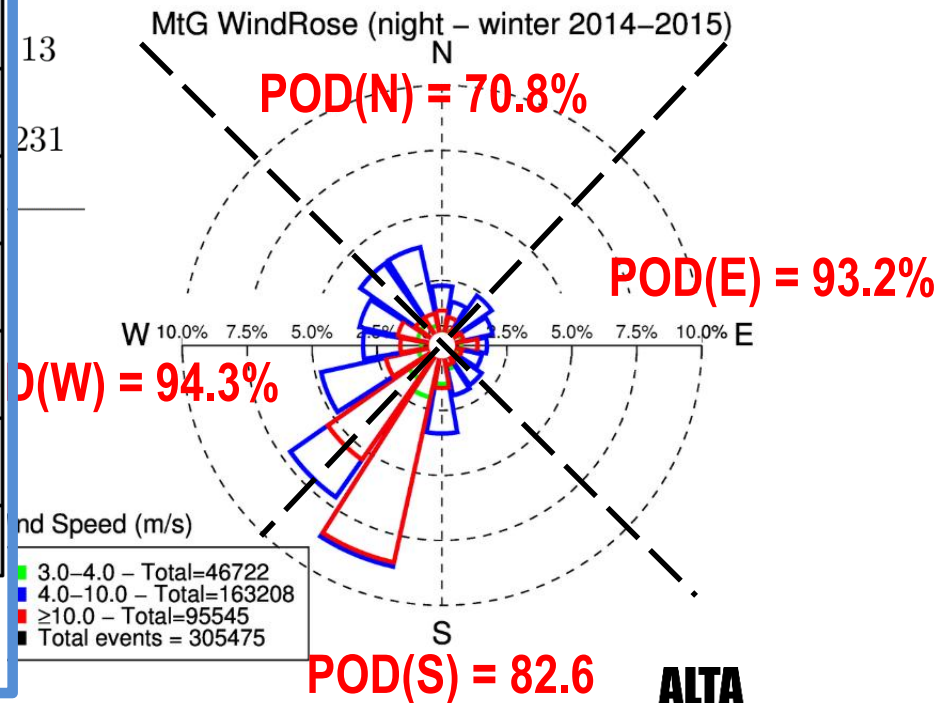
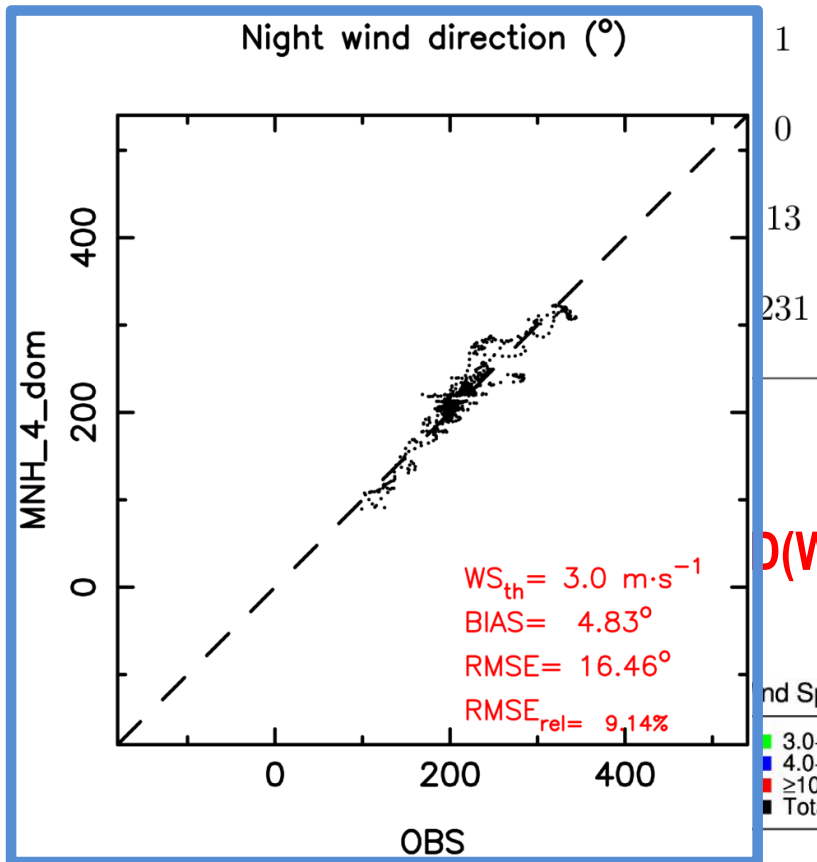


# Wind direction $\Delta X=100m$

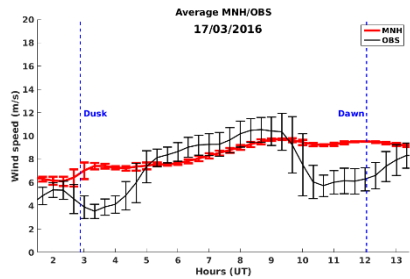
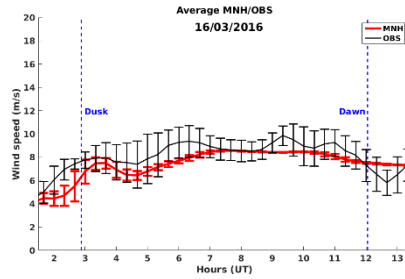
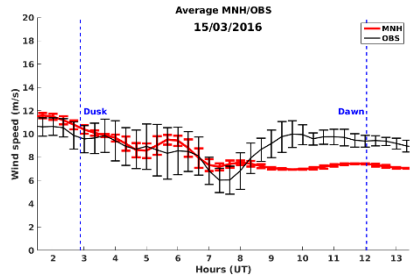
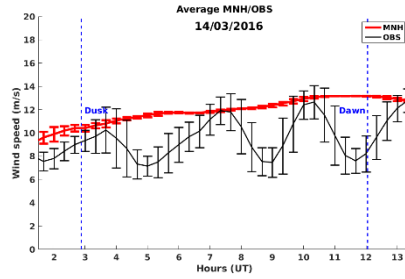
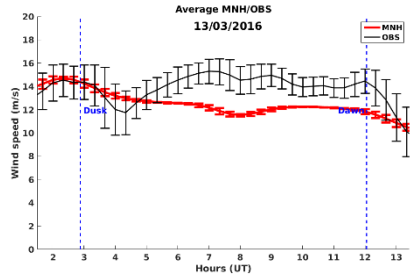
WIND DIRECTION contingency table,  $\Delta X=100m$

MtG - 58m	OBSERVATIONS			
	N	E	S	W

**PC = 85.8%**  
**EBD = 0%**

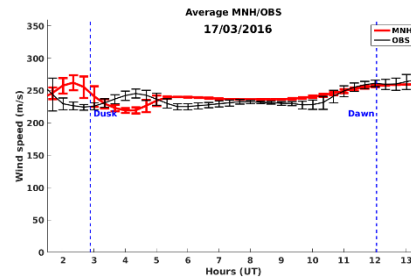
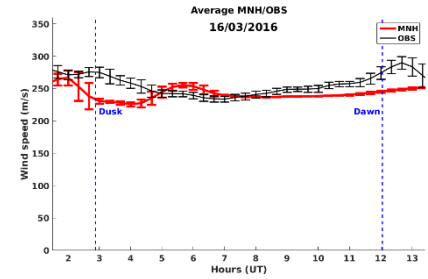
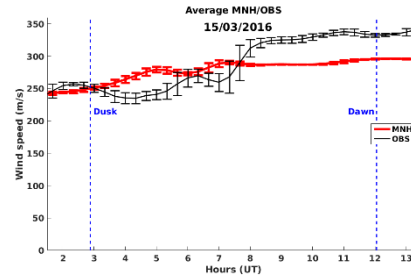
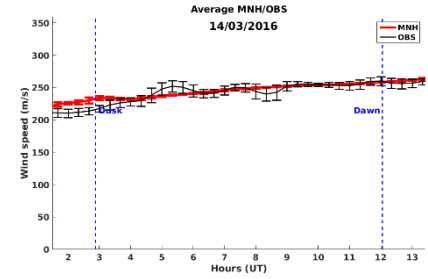
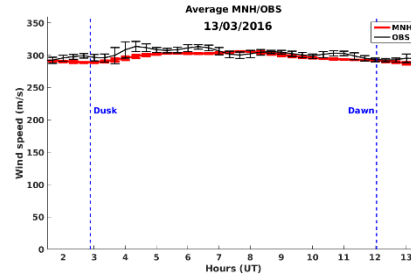


# Use case: ARGOS run 13/03/2016 – 17/03/2016 (UT)



## Wind speed

BIAS = -1.2 m/s  
 RMSE = 2.0 m/s  
 $\sigma$  = 1.6 m/s



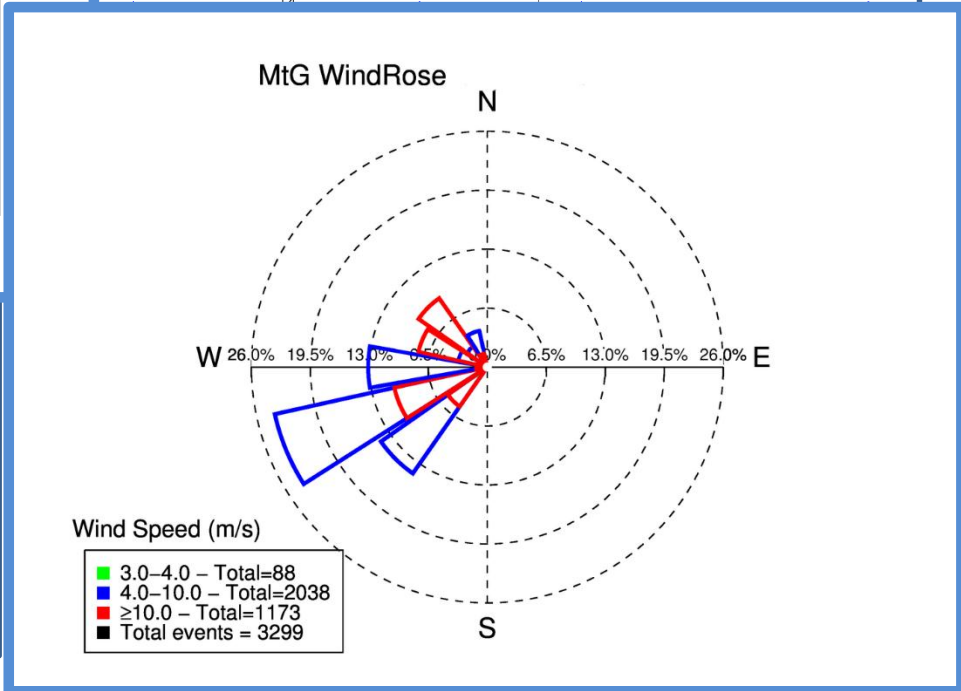
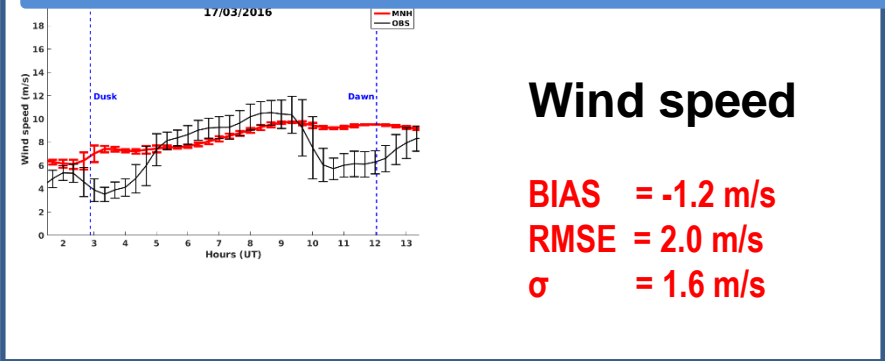
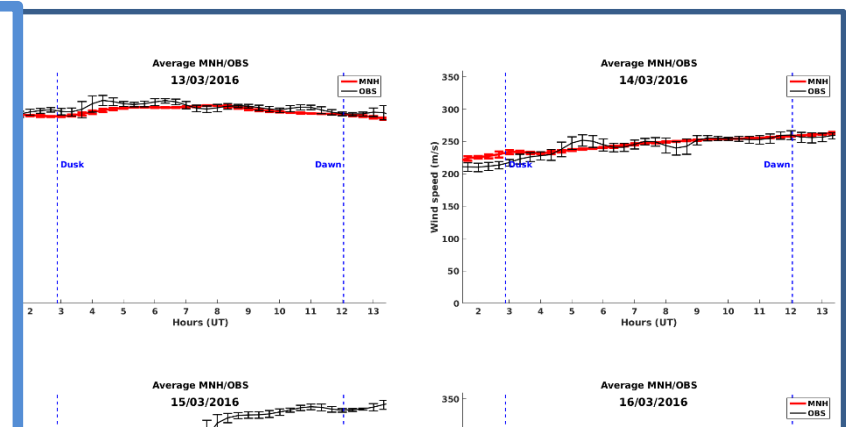
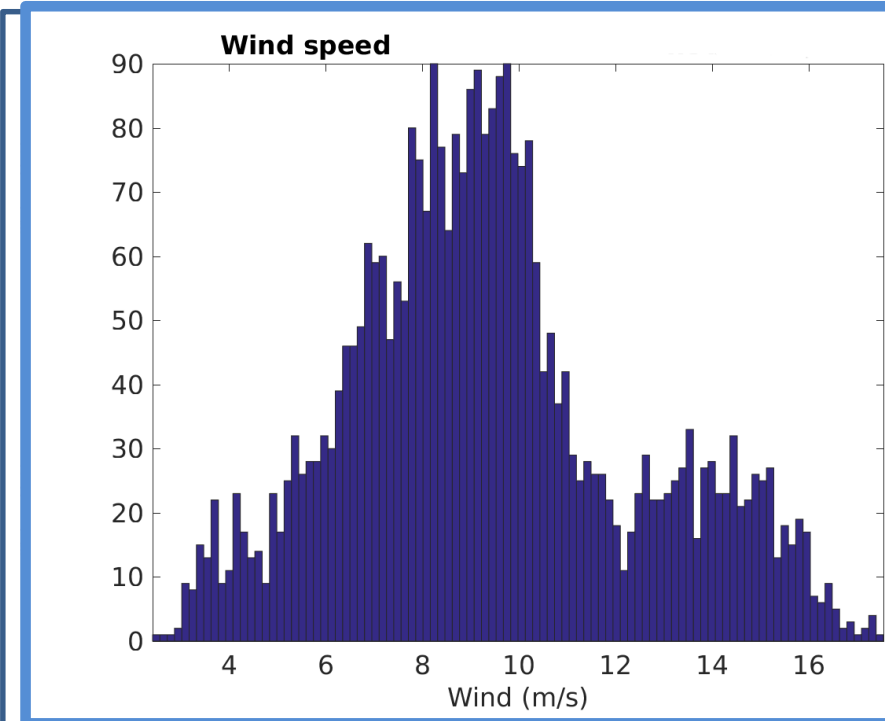
## Wind direction

BIAS = 3.0 °  
 RMSE = 20.2 °  
 RMSE(rel) = 11.2%





# Use case: ARGOS run 13/03/2016 – 17/03/2016 (UT)



# Conclusions

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1. We build an operational forecast model configuration for the LBT site, testing multiple possible solutions. The setup proves to be efficient and able to run within the project's constraints.
2. We started an preliminary validation test on all the possible tested setups, using the telemetry measures taken from LBT instrumentation above the dome. Initial results from the ongoing validation test allowed us to select the best possible configuration. The results for ground weather parameters shown in this contribution show an excellent level of model performance.
3. The sample size will be increased to a richer statistical ensemble of ~140 nights, in order to confirm the validity of the measured performance , however the overall performance is already on par with the state of the art for other sites (e.g. Paranal, Cerro Armazones).

Masciari et al., MNRAS 2013; Lascaux et al., MNRAS 2013; Lascaux et al., MNRAS 2015

